## *INTRODUCTION*



the Free Field method. The sound pressure level of a product is measured using one of these test methods. A calculation is then used to convert the measured sound pressure levels to sound power levels.

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### *ATTENUATOR INFORMATION*

### STATIC INSERTION LOSSES

BS 4718 : 1971 "Methods of Test for Attenuators for Air Distribution Systems" requires manufacturers to test and publish static insertion loss figures.

An insertion loss is defined as "the reduction in noise level at a given location due to the placement of an attenuator in the sound path between the sound source and that location". A static insertion loss is the insertion loss with no air flow passing through the attenuator.

Therefore placing an attenuator in between a fan and the measuring position, will reduce the noise level at the measuring position by the insertion loss.

### DYNAMIC INSERTION LOSSES

Fantech test attenuators to BS4718: 1971 "Methods of Test for Attenuators for Air Distribution Systems". This test standard sets out a procedure for the testing of static insertion losses; i.e. the measuring of insertion losses without air flow.

Some overseas companies publish dynamic insertion losses; that is the testing of insertion losses with air flow involved. At higher passage velocities the static insertion loss can vary from the dynamic insertion loss by a small margin, depending on the direction of the air flow compared to the noise propagation direction.

For typical velocities associated with a HVAC system, the static insertion losses and dynamic insertion losses are virtually identical and can be assumed to be the same.

### AIRWAY VELOCITY

For a given attenuator size a higher air flow results in a higher airway passage velocity. Higher passage velocities will increase the regenerated noise level of the attenuator. This is particularly critical when the attenuator is serving a low noise level zone; i.e. film studio. A number of suggested maximum passage velocities with the appropriate room NR level are tabulated. Critical noise applications should be checked by an Acoustics Engineer.



Critical noise level application should be checked by an acoustics engineer

### TYPICAL APPLICATIONS AND BENEFITS OF ATTENUATOR TYPES



\*NTA/NSA AirLay series are suitable for temperatures up to 80°C and dry applications only.

### *NOISE RATINGS*

### dB(A) LEVELS

The ear responds not only to the absolute sound pressure level of a sound, but also to its frequency content. It actually gives a weighting to the level of sound according to its frequency content, and ascribes a certain loudness. This means that if we want to know how a person will judge the sound, we must somehow translate our objective measured units of sound pressure level and frequency content into subjective units of loudness.

A sound level meter accepts all of the frequency components of a sound, and adds all their absolute levels together to give an overall sound pressure level, dB (Linear).

The illustration below shows typical overall sound pressure levels produced by some everyday sources.



However the ear is not as sensitive to lower frequency sound pressure levels as it is to higher frequency sound pressure levels. In the 1930's, experiments were carried out on 11 people by Harvey Fletcher at the Bell Telephone Laboratories in New York to determine how loud tones of different frequencies sounded subjectively. Therefore the "A" weighting (or the "A" in dB(A)) was devised so that the sound meter would filter each frequency of sound by a certain amount before adding them together to give a loudness that more closely follows the sensitivity of the human ear.



The 'A' frequency weighting corrections are shown below.

The 'A' frequency weighting suggests that if a tone of 40 dB is played at 1000 Hz, a 40 dB tone played at 63 Hz would sound 26 dB quieter, or be 14 dB(A). Due to its simplicity and convenience, the 'A' frequency weighting has become popular and is now used for many different noise sources at different levels. In fact, most legislation regarding noise is written using dB(A)s, in addition nearly all manufacturers of fans and other noise generating machines quote their noise levels in dB(A)s at 1, 1.5, or 3 metres assuming spherical distribution. It is therefore important that we understand the 'A' frequency weighting and how dB(A)s are calculated.

### CALCULATING dB(A) LEVELS

Published dB(A), or 'A' frequency weighted, sound pressure levels are theoretical values. These are, in fact, calculated from the sound power level data and are quoted at a specified distance i.e. 1, 1.5, or 3 metres. For example, using the Fantech model AP0804AP10/23 (duty 7000 L/s @ 80 Pa, inlet side), by applying an 'A' frequency weighting correction to the fan sound power levels for each frequency and then logarithmically adding the values from left to right the resultant overall sound power level for this unit will be 98 dB(A). A further calculation is required to convert this value from the 'A' weighted sound power level to an 'A' weighted sound pressure level at a prescribed distance from the noise source i.e. 77 dB(A)  $@$  3m.

See next page for a detailed example of this calculation.

### dB(A) CALCULATION EXAMPLE

#### **1. 'A' weighting corrections**



#### **2. Calculating an overall sound level**

For each sound power level:

- a. Calculate the difference between the sound power level and the sub total.
- b. Refer to the Decibels dB(A) diagram on the previous page to determine the value to add.
- c. Add the value to add to the highest of the sub total and the sound power level.



98.2 dB(A) is rounded to 98 dB(A).

#### **3. Converting Sound Power to Sound Pressure**

To convert this 'A' weighted sound "power" level to an 'A' weighted sound "pressure" level (which is calculated for a specified distance from the source) the following equation is used:  $L_p = L_w - 20 log_{10}(d) - 11$ 

Where:

 $L_W$  = Sound Power Level re 10<sup>-12</sup>W (dB)  $L_{\text{D}} =$  Sound Pressure Level re 20µPa (dB)  $d =$  Distance from fan in metres (m) Therefore, to determine the  $L_p = 98 - 10.5 - 11$ dB(A) sound  $L_p = 98 - 20 log_{10} (3) - 11$ 

pressure level  $L_p = 98 - 21$ at a distance of  $L_p = 77$  dB(A) @ 3m 3m:

### NR & PNC Ratings

The Noise Rating (or NR Contour) curves were proposed by Kosten and Van Os (1962) to rate internal noise levels. Some acoustic consultants preter to use the Preferred Noise Criterion (PNC) curves. These were designed by Beranek (1971) to achieve more acceptable noise quality and lower allowable levels of low and high frequency noises. They are designed to be used with broadband constant noise sourced (eg. motors, engines), and do not allow for the increased annoyance associated with tonal, or pulsating noises.

NR or PNC levels are only applicable to a space/room and not to a piece of equipment. When a consultant specifies a target NR or PNC level in a space, an acoustic analysis is required that considers the complete system including the selected fan, attenuator, duct, and fittings, in order to determine if the

designed system will meet this target. As a rule of thumb to determine the approximate equivalent maximum dB(A) level within the space/room add 5 to the NR or PNC value.

It is therefore important to understand that a fans sound power level spectrum cannot be used to determine a NR or PNC value on the curves below, nor can a fans  $dB(A)$  @ 3m value be converted to a NR or PNC value.

To use the curves, plot the noise spectrum within the space from the resulting acoustic analysis onto the NR or PNC curves grid. The curve which covers all points of the plotted spectrum is the NR or PNC value. IN the examples below, the NR rating is 40, and the PNC rating is 50.



### ATTENUATOR AIRWAY VELOCITY

For industrial applications and to determine attenuator re-generated noise, the airway velocity must be found as described below:



### ATTENUATOR RE-GENERATED/ AIR FLOW GENERATED NOISE :

As air passes through an attenuator it will frequently pass at speeds as much as 2 to 4 times the air flow speed in the duct. Moving air creates noise, so in noise sensitive rooms and installations where attenuators are placed close to air grilles and terminals, particular care must be taken to ensure that this does not become the dominating noise source. The relationship between airway velocity and generated noise is shown below for rectangular attenuators.



### **Airway Velocity m/sec 63 125 250 500 1k 2k 4k 8k <8** -2 -6 -7 -10 -12 -16 -19 -22  $\geq$ **8 &**  $\leq$ **32** -3 -5 -8 -7 -8 -10 -13 -15 **>32** -3 -6 -10 -7 -7 -8 -10 -12 **Octave Band Centre Frequency, Hz**

### SPECTRUM CORRECTIONS FOR AIRWAY VELOCITY :

### REFERENCE INFORMATION: ACOUSTIC LOSSES OF LINED DUCT & BENDS

### Table 1: 25mm lined duct

# **Insertion Loss, dB/metre**

## **Insertion Loss, dB/metre** Table 2: 50mm lined duct

**Width** 



#### Table 3: Square lined bend with turning vanes **Insertion Loss, dB/bend Octave Band Centre Frequency (Hz)**





#### Table 4: Square lined bend without turning vanes **Insertion Loss, dB/bend Octave Band Centre Frequency (Hz)**



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